STORMWATER REPORT

79 Hill Street Topsfield, Massachusetts

February 15, 2023 Revised: August 4, 2023

> Applicant: Barbara Crowley 15 Timber Lane Topsfield, MA 01983

Prepared By Williams & Sparages, LLC 189 North Main Street, Suite 101 Middleton, MA 01949 Ph: 978-539-8088 Fax: 978-539-8200 www.wsengineers.com

W&S Project Data

TOPS-0077
Shill#79.dwg
EXISTING.hcp
PROPOSED.hcp
p:\TOPS-0077(79 Hill Street)\drainage\stormwater_report.docx



Project Narrative

The subject property is located at 79 Hill Street in Topsfield located within the O-R-A Zoning District. It is currently an undeveloped lot covered by trees and undergrowth with remains of old foundations and stone walls present on the lot.

The proposal is to construct a four-bedroom (9 Habitable Room Max.) single family house on the lot. Coinciding with this proposal will be the construction of a paved driveway, regrading a portion of the lot, a proposed septic system and proposed stormwater management area to capture roof runoff.

Peak Rate Runoff Tables

Examining the following Peak Rate/Volume of Runoff and Basin Performance table, the proposed stormwater management system is effective for mitigating the peak flow rates from the limit of watershed analysis for the 2-year, 10-year and 100-year storm events using the NOAA-14 Atlas Point Precipitation Frequency Estimates in order to be conservative. See attached table.

Total Peak Runoff Tables

Table 1.0: Total Peak Rate of Runoff Comparison Location 1L						
Description	2 Year	10 Year		100 Year		
Existing Peak						
Rate of Runoff	1.23	3.29		7.18		
(cfs)						
Proposed Peak						
Rate of Runoff	1.20	3.08		6.52		
(cfs)						
Difference	-0.03	-0.21		-0.66		

Table 1.1: Total Peak Volume of Runoff Comparison Location 1L						
Description	2 Year	10 Year	100 Year			
Existing Peak						
Volume of	6,247	15,447	32,942			
Runoff (cf)						
Proposed Peak						
Volume of	5,814	13,896	29,363			
Runoff (cf)						
Difference	-433	-1,51	-3,579			

Drawdown Within 72 Hours:

 $T_{drawdown} = [R_{v \text{ total}} / (K)(Bottom Area)]$

Stormwater Management Area 1P - Rear 1/2 of Roof Recharge System

 $R_{v 1P}$ = 827 ft³ (peak volume in 100yr storm to be conservative)

K = 1.02 in/hr (Rawls Rate)

Bottom Area = 275 ft^2

 $T_{drawdown} = 827 / [(1.02)(275)/12] = 35.4 \text{ hours} < 72 \text{ hours}$

Stormwater Management Area 2P - Stormwater Management Area for front ½ roof, driveway & front yard

 $R_{v 2P} = 3.984 \text{ ft}^3 \text{ (peak volume in 100yr storm)}$

K = 1.02 in/hr (Rawls Rate)

Bottom Area = 1150 ft²

 $T_{drawdown} = 3984 / [(1.02)(1150) / 12] = 40.7 \text{ hours} < 72 \text{ hours}$

Recharge Volume:

 $R_{v \text{ required}} = \text{(Impervious Area)} (F)$

Site consists of Hydrologic Soils Group C: $F_C = 0.25$ in.

Site Impervious Area Draining to Recharge Facilities:

Stormwater Management Area 1P-Roof Recharge System

 $A_{\text{imp C soils}} = 1391 \text{ ft}^2$

 $R_{\text{v required}} = [(1391) (0.25)/12] = 29.0 \text{ ft}^3$

 $R_{v \text{ provided}} = 545 \text{ ft}^3$; Therefore Okav

Stormwater Management Area 2P Stormwater Management Area for front 1/2 driveway & front yard

 $A_{\text{imp C soils}} = 5739 \text{ ft}^2$

 $R_{\text{v required}} = [(5739) (0.25)/12] = 119.6 \text{ ft}^3$

 $R_{v \text{ provided}}$ = 6990 ft³ below outlet; Therefore Okay

Water Quality Volume:

 $V_{\text{wq required}} = (A_{\text{imp}})(D_{\text{wq}})$

 $D_{WO} = 0.5 \text{ in}$

Stormwater Management Area 1P- Rear ½ Roof Recharge System

 $V_{\text{wq required}} = [(0) (0.5)/12] = 0 \text{ ft}^3$

Exempt from this requirement, roof runoff only considered clean by DEP for certain types

Stormwater Management Area 1P- Stormwater Management Area for front ½ roof, driveway & front yard

 $V_{\text{wq required}} = [(4419) (0.5)/12] = 184.1 \text{ ft}^3$

 $V_{\text{wq provided}} = 3717 \text{ ft}^3 \text{ below outlet; Therefore Okay}$

Front ½ roof Exempt from this requirement, roof runoff only considered clean by DEP for certain types



Mitigative Drainage Analysis 79 Hill Street | Topsfield, MA

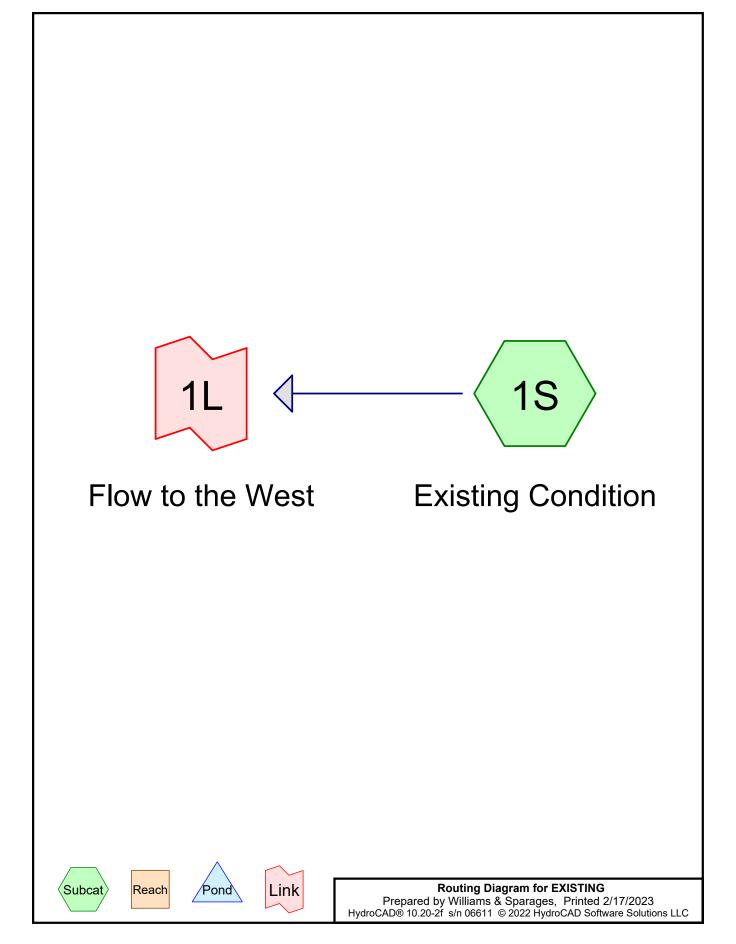
Revised: August 4, 2023

HydroCAD Data

Mitigative Drainage Analysis 79 Hill Street | Topsfield, MA

79 Hill Street | Topsfield, MA Revised: August 4, 2023

Existing Condition - No Change



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Rainfall Events Listing (selected events)

Event#	Event	Storm Type	Curve	Mode	Duration	B/B	Depth	AMC
	Name				(hours)		(inches)	
1	2-yr	Type III 24-hr		Default	24.00	1	3.29	2
2	10-yr	Type III 24-hr		Default	24.00	1	5.19	2
3	100-yr	Type III 24-hr		Default	24.00	1	8.21	2

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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
2,375	74	>75% Grass cover, Good, HSG C (1S)
82,722	70	Woods, Good, HSG C (1S)
85,097	70	TOTAL AREA

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
0	HSG B	
85,097	HSG C	1S
0	HSG D	
0	Other	
85.097		TOTAL AREA

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Summary for Subcatchment 1S: Existing Condition

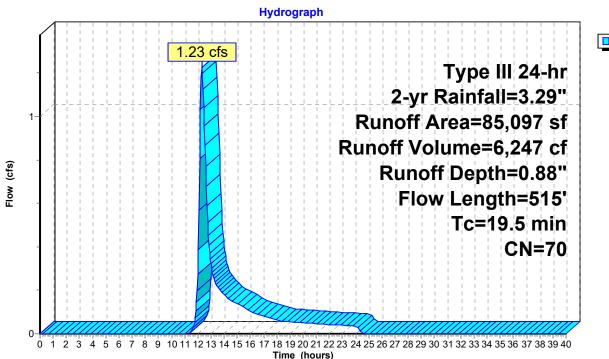
Runoff = 1.23 cfs @ 12.31 hrs, Volume= 6,247 cf, Depth= 0.88"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Rainfall=3.29"

	Α	rea (sf)	CN	Description						
		82,722								
_		2,375	74	>75% Gras	s cover, Go	ood, HSG C				
		85,097	70	Weighted A	verage					
		85,097		100.00% Pe	ervious Are	a				
	Tc	Length	Slope	•	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	13.0	100	0.0680	0.13		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.28"				
	6.5	415	0.0450	1.06		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
-	19.5	515	Total	•	•					

Subcatchment 1S: Existing Condition





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Summary for Link 1L: Flow to the West

85,097 sf, 0.00% Impervious, Inflow Depth = 0.88" for 2-yr event Inflow Area =

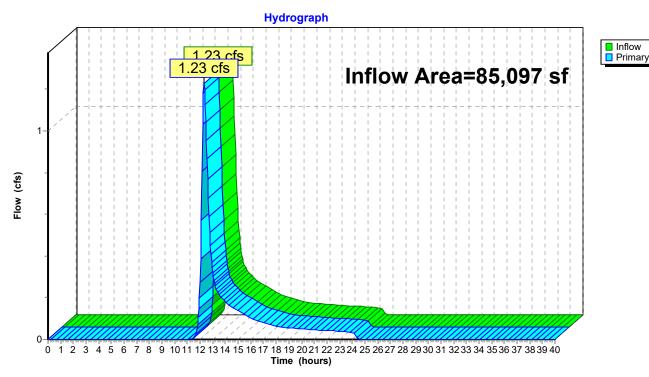
Inflow 6,247 cf

1.23 cfs @ 12.31 hrs, Volume= 1.23 cfs @ 12.31 hrs, Volume= 6,247 cf, Atten= 0%, Lag= 0.0 min Primary

Routed to nonexistent node 3L

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs

Link 1L: Flow to the West



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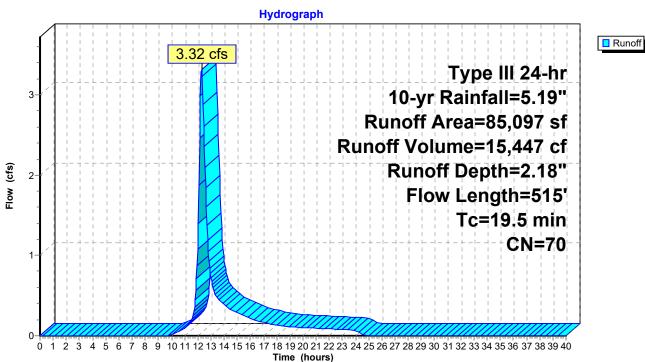
Summary for Subcatchment 1S: Existing Condition

Runoff = 3.32 cfs @ 12.28 hrs, Volume= 15,447 cf, Depth= 2.18" Routed to Link 1L : Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Rainfall=5.19"

	Α	rea (sf)	CN	Description						
		82,722								
_		2,375	74	>75% Gras	s cover, Go	ood, HSG C				
		85,097	70	Weighted A	verage					
		85,097		100.00% Pe	ervious Are	a				
	Tc	Length	Slope	•	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	13.0	100	0.0680	0.13		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.28"				
	6.5	415	0.0450	1.06		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
-	19.5	515	Total	•	•					

Subcatchment 1S: Existing Condition



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Summary for Link 1L: Flow to the West

85,097 sf, 0.00% Impervious, Inflow Depth = 2.18" for 10-yr event Inflow Area =

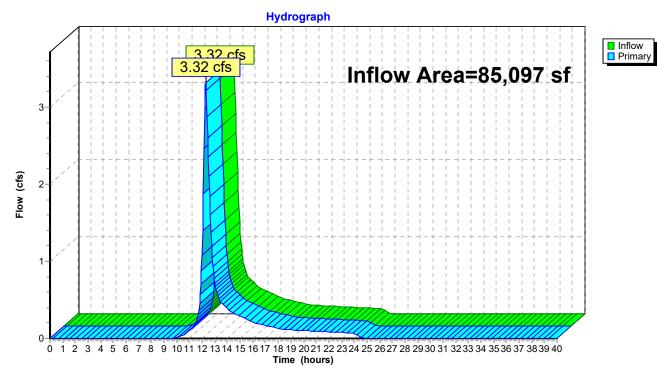
Inflow 15,447 cf

3.32 cfs @ 12.28 hrs, Volume= 3.32 cfs @ 12.28 hrs, Volume= 15,447 cf, Atten= 0%, Lag= 0.0 min Primary

Routed to nonexistent node 3L

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs

Link 1L: Flow to the West



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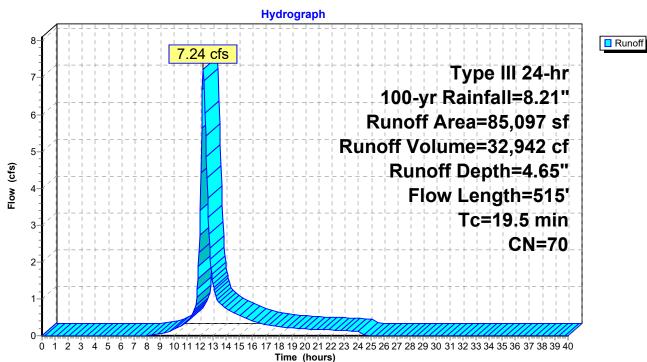
Summary for Subcatchment 1S: Existing Condition

Runoff = 7.24 cfs @ 12.27 hrs, Volume= 32,942 cf, Depth= 4.65" Routed to Link 1L : Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 100-yr Rainfall=8.21"

	Α	rea (sf)	CN E	Description							
		82,722	70 V	70 Woods, Good, HSG C							
		2,375	74 >	75% Gras	s cover, Go	ood, HSG C					
		85,097	70 V	Veighted A	verage						
		85,097	1	00.00% Pe	ervious Are	a					
	Tc	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	13.0	100	0.0680	0.13		Sheet Flow,					
						Woods: Light underbrush n= 0.400 P2= 3.28"					
	6.5	415	0.0450	1.06		Shallow Concentrated Flow,					
_						Woodland Kv= 5.0 fps					
	19.5	515	Total								

Subcatchment 1S: Existing Condition



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Summary for Link 1L: Flow to the West

85,097 sf, 0.00% Impervious, Inflow Depth = 4.65" for 100-yr event Inflow Area =

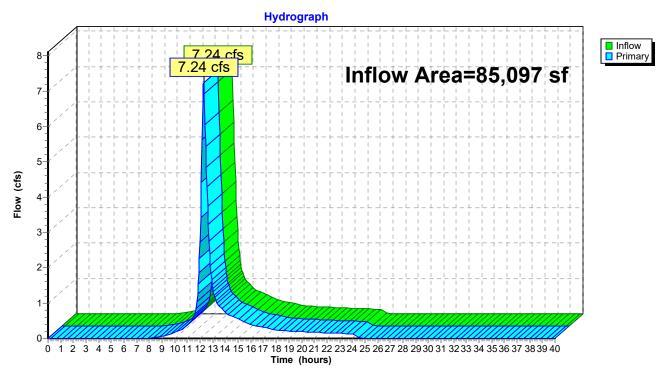
Inflow 32,942 cf

7.24 cfs @ 12.27 hrs, Volume= 7.24 cfs @ 12.27 hrs, Volume= 32,942 cf, Atten= 0%, Lag= 0.0 min Primary

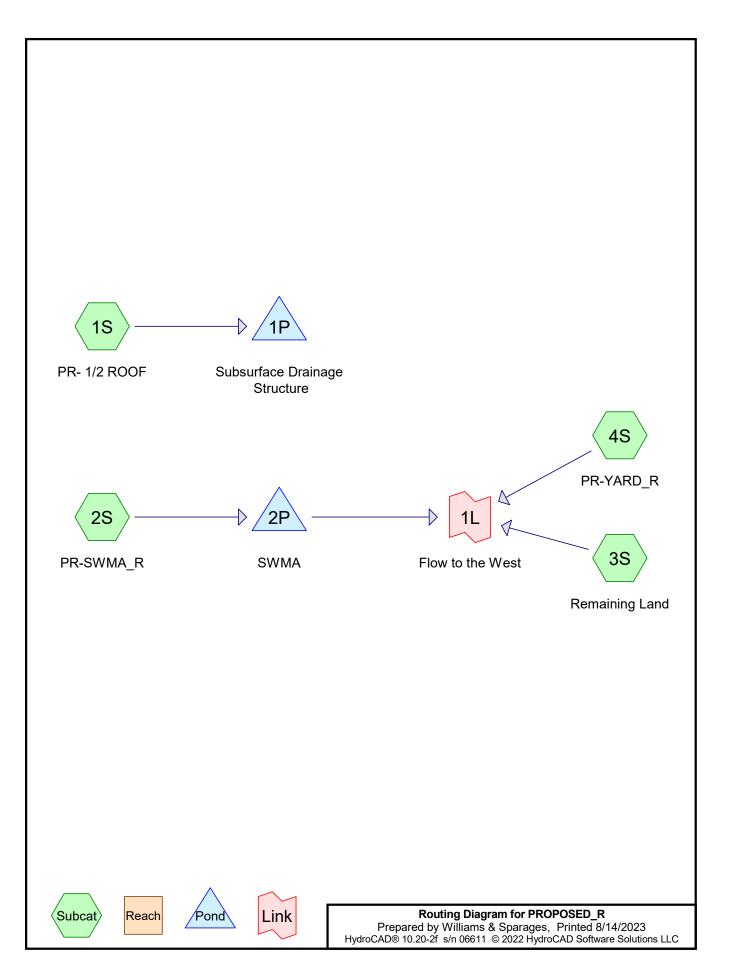
Routed to nonexistent node 3L

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs

Link 1L: Flow to the West



Proposed Condition



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Project Notes

Defined 4 rainfall events from MA-Topsfield IDF

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Rainfall Events Listing (selected events)

Event	# Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
	1 2-yr	Type III 24-hr		Default	24.00	1	3.29	2
2	2 10-yr	Type III 24-hr		Default	24.00	1	5.19	2
;	3 100-yr	Type III 24-hr		Default	24.00	1	8.21	2

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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
37,964	74	>75% Grass cover, Good, HSG C (2S, 3S, 4S)
4,410	98	Paved parking, HSG C (2S)
1,391	98	Roofs, HSG C (1S)
1,329	98	Unconnected roofs, HSG C (2S)
40,003	70	Woods, Good, HSG C (3S, 4S)
85,097	74	TOTAL AREA

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Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
0	HSG B	
85,097	HSG C	1S, 2S, 3S, 4S
0	HSG D	
0	Other	
85.097		TOTAL AREA

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Ground Covers (all nodes)

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
 (sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
0	0	37,964	0	0	37,964	>75% Grass
						cover, Good
0	0	4,410	0	0	4,410	Paved parking
0	0	1,391	0	0	1,391	Roofs
0	0	1,329	0	0	1,329	Unconnected
						roofs
0	0	40,003	0	0	40,003	Woods, Good
0	0	85,097	0	0	85,097	TOTAL AREA

Proposed Condition Watershed Analysis Revised August 4, 2023

PROPOSED_R

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Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
1	2P	99.25	98.00	45.0	0.0278	0.010	0.0	4.0	0.0

Proposed Condition Watershed Analysis Revised August 4, 2023

Type III 24-hr 2-yr Rainfall=3.29"

PROPOSED_R

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Time span=0.00-40.00 hrs, dt=0.05 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: PR- 1/2 ROOF Runoff Area=1,391 sf 100.00% Impervious Runoff Depth=3.06"

Tc=6.0 min CN=98 Runoff=0.10 cfs 354 cf

Subcatchment 2S: PR-SWMA_R Runoff Area=11,800 sf 48.64% Impervious Runoff Depth=1.91"

Tc=6.0 min CN=86 Runoff=0.60 cfs 1,882 cf

Subcatchment 3S: Remaining Land Runoff Area=31,753 sf 0.00% Impervious Runoff Depth=0.88"

Flow Length=345' Tc=21.3 min CN=70 Runoff=0.44 cfs 2,331 cf

Subcatchment 4S: PR-YARD R Runoff Area=40,153 sf 0.00% Impervious Runoff Depth=1.04"

Flow Length=345' Slope=0.0350 '/' Tc=12.1 min CN=73 Runoff=0.85 cfs 3,483 cf

Pond 1P: Subsurface Drainage Structure Peak Elev=90.41' Storage=143 cf Inflow=0.10 cfs 354 cf

Outflow=0.01 cfs 354 cf

Pond 2P: SWMA Peak Elev=97.70' Storage=905 cf Inflow=0.60 cfs 1,882 cf

Discarded=0.03 cfs 1,882 cf Primary=0.00 cfs 0 cf Outflow=0.03 cfs 1,882 cf

Link 1L: Flow to the West Inflow=1.20 cfs 5,814 cf

Primary=1.20 cfs 5,814 cf

Total Runoff Area = 85,097 sf Runoff Volume = 8,050 cf Average Runoff Depth = 1.14" 91.62% Pervious = 77,967 sf 8.38% Impervious = 7,130 sf HydroCAD® 10.20-2f s/n 06611 © 2022 HydroCAD Software Solutions LLC

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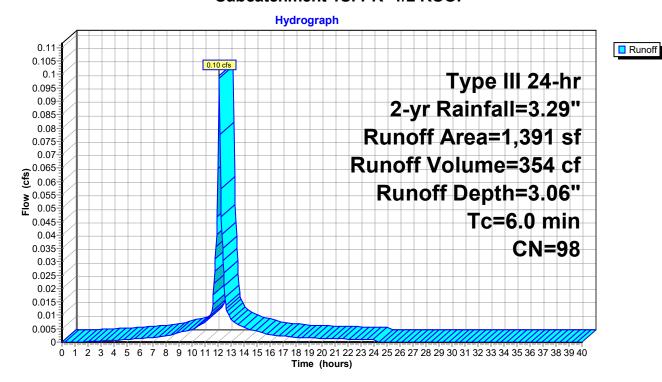
Summary for Subcatchment 1S: PR- 1/2 ROOF

Runoff = 0.10 cfs @ 12.09 hrs, Volume= 354 cf, Depth= 3.06" Routed to Pond 1P : Subsurface Drainage Structure

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Rainfall=3.29"

A	rea (sf)	CN [Description		
	1,391	98 F	Roofs, HSC	G C	
	1,391	1	100.00% Im	npervious A	Area
Tc	U	Slope	•		Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0					Direct Entry,

Subcatchment 1S: PR- 1/2 ROOF



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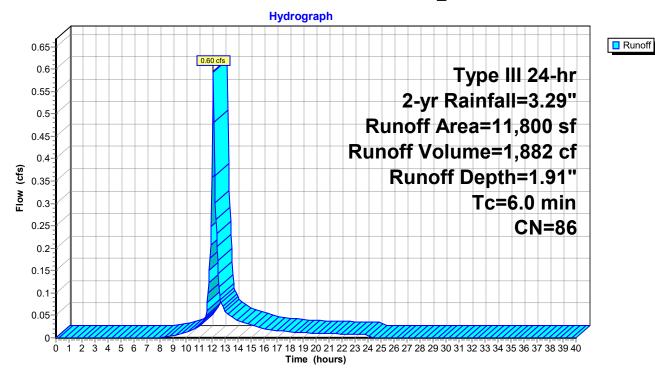
Summary for Subcatchment 2S: PR-SWMA_R

Runoff = 0.60 cfs @ 12.09 hrs, Volume= 1,882 cf, Depth= 1.91" Routed to Pond 2P : SWMA

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Rainfall=3.29"

Aı	rea (sf)	CN	Description					
	4,410	98	Paved park	ing, HSG C	C			
	6,061	74	>75% Ġras	s cover, Go	Good, HSG C			
	1,329	98	Unconnecte	ed roofs, H	ISG C			
•	11,800	86	Weighted A	verage				
	6,061		51.36% Pervious Area					
	5,739		48.64% Impervious Area					
	1,329		23.16% Unconnected					
Tc	Longth	Slope	Volocity	Canacity	Description			
	Length	Slope	,	Capacity	•			
<u>(min)</u>	(feet)	(ft/ft	(ft/sec)	(cfs)				
6.0					Direct Entry,			

Subcatchment 2S: PR-SWMA_R



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Runoff

Summary for Subcatchment 3S: Remaining Land

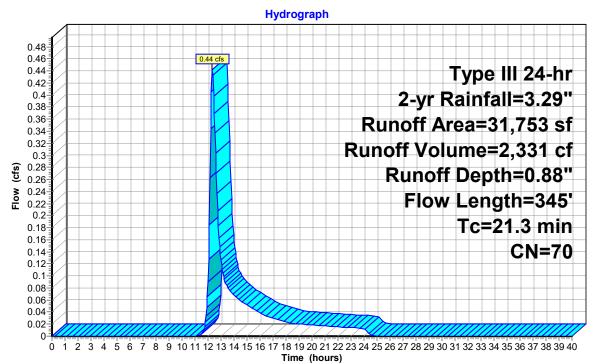
Runoff = 0.44 cfs @ 12.33 hrs, Volume= 2,331 cf, Depth= 0.88"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Rainfall=3.29"

	rea (sf)	CN [Description					
	30,003	70 \	Woods, Good, HSG C					
	1,750	74 >	>75% Gras	s cover, Go	ood, HSG C			
	31,753	70 \	Weighted Average					
	31,753	•	100.00% Pervious Area					
Tc	Length	Slope		Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
17.0	100	0.0350	0.10		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.28"			
4.3	245	0.0360	0.95		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
21.3	345	Total						

Subcatchment 3S: Remaining Land



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Runoff

Summary for Subcatchment 4S: PR-YARD_R

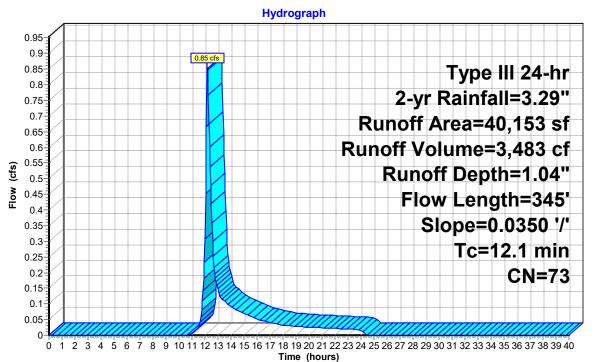
Runoff = 0.85 cfs @ 12.18 hrs, Volume= 3,483 cf, Depth= 1.04"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 2-yr Rainfall=3.29"

	Area (sf)	CN I	Description					
	30,153	74	>75% Grass cover, Good, HSG C					
	10,000	70 \	Noods, Go	od, HSG C				
	40,153	73 \	Weighted Average					
	40,153		100.00% Pervious Area					
Tc	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
7.7	100	0.0350	0.22		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.28"			
4.4	245	0.0350	0.94		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
12.1	345	Total						

Subcatchment 4S: PR-YARD_R



PROPOSED R

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Summary for Pond 1P: Subsurface Drainage Structure

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=9)

Inflow Area = 1,391 sf,100.00% Impervious, Inflow Depth = 3.06" for 2-yr event

Inflow = 0.10 cfs @ 12.09 hrs, Volume= 354 cf

Outflow = 0.01 cfs @ 11.45 hrs, Volume= 354 cf, Atten= 94%, Lag= 0.0 min

Discarded = 0.01 cfs @ 11.45 hrs, Volume= 354 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Peak Elev= 90.41' @ 13.58 hrs Surf.Area= 274 sf Storage= 143 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 171.0 min (926.8 - 755.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	89.50'	253 cf	11.17'W x 24.50'L x 3.54'H Field A
			969 cf Overall - 335 cf Embedded = 634 cf x 40.0% Voids
#2A	90.00'	335 cf	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		589 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	89.50'	1.020 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.01 cfs @ 11.45 hrs HW=89.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.01 cfs)

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Pond 1P: Subsurface Drainage Structure - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

3 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 22.50' Row Length +12.0" End Stone x 2 = 24.50' Base Length

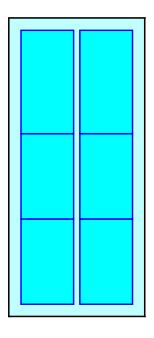
2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

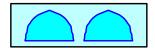
6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 335.3 cf Chamber Storage

968.9 cf Field - 335.3 cf Chambers = 633.6 cf Stone x 40.0% Voids = 253.5 cf Stone Storage

Chamber Storage + Stone Storage = 588.8 cf = 0.014 af Overall Storage Efficiency = 60.8% Overall System Size = 24.50' x 11.17' x 3.54'

6 Chambers 35.9 cy Field 23.5 cy Stone

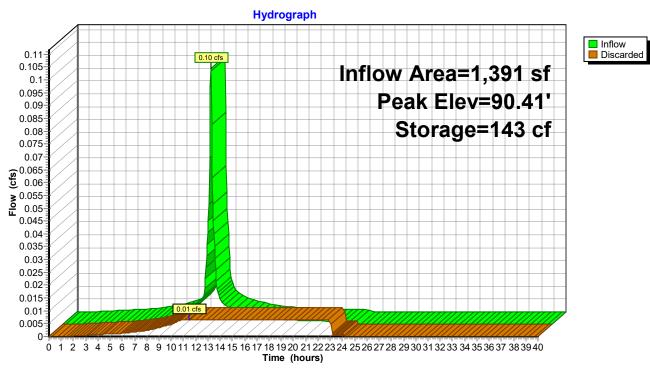




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Pond 1P: Subsurface Drainage Structure



Volume

Type III 24-hr 2-yr Rainfall=3.29"

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Summary for Pond 2P: SWMA

11,800 sf, 48.64% Impervious, Inflow Depth = 1.91" for 2-yr event Inflow Area = 0.60 cfs @ 12.09 hrs, Volume= Inflow 1.882 cf 0.03 cfs @ 14.39 hrs, Volume= 1,882 cf, Atten= 94%, Lag= 138.0 min Outflow 0.03 cfs @ 14.39 hrs, Volume= Discarded = 1,882 cf

Primary 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routed to Link 1L: Flow to the West

Invort

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Peak Elev= 97.70' @ 14.39 hrs Surf.Area= 1,449 sf Storage= 905 cf

Avail Storage Storage Description

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 269.6 min (1,090.9 - 821.3)

volume	invert	Avaii.Sto	rage Storage L	pescription	
#1	97.00'	6,99	90 cf Custom S	Stage Data (Pris	smatic) Listed below (Recalc)
Elevation		ırf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
97.0	00	1,150	0	0	
98.0	00	1,580	1,365	1,365	
99.0	00	2,060	1,820	3,185	
100.0	00	2,600	2,330	5,515	
100.5	50	3,300	1,475	6,990	
Device	Routing	Invert	Outlet Devices		
#1	Discarded	97.00'	1.020 in/hr Exf	iltration over S	urface area
#2	Primary	99.25'	4.0" Round C	ulvert	
			·	vert= 99.25' / 98	eadwall, Ke= 0.500 3.00' S= 0.0278 '/' Cc= 0.900

Discarded OutFlow Max=0.03 cfs @ 14.39 hrs HW=97.70' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

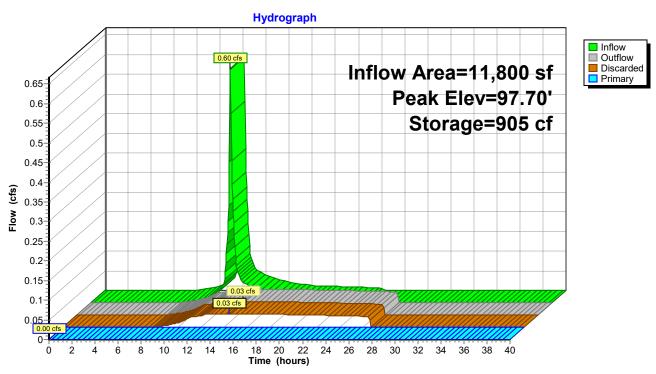
Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=97.00' TW=0.00' (Dynamic Tailwater) 2=Culvert (Controls 0.00 cfs)

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Pond 2P: SWMA



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Summary for Link 1L: Flow to the West

Inflow Area = 83,706 sf, 6.86% Impervious, Inflow Depth = 0.83" for 2-yr event

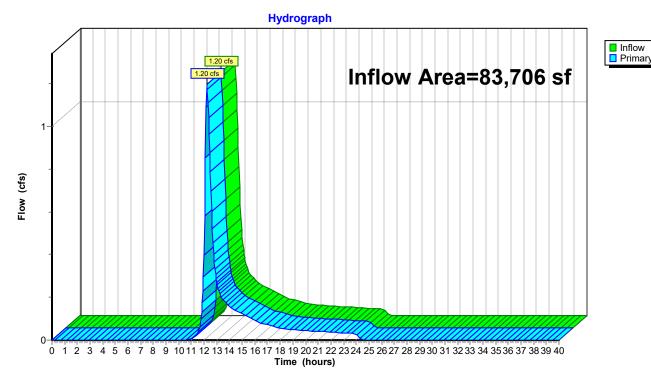
Inflow = 1.20 cfs @ 12.22 hrs, Volume= 5,814 cf

Primary = 1.20 cfs @ 12.22 hrs, Volume= 5,814 cf, Atten= 0%, Lag= 0.0 min

Routed to nonexistent node 3L

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs

Link 1L: Flow to the West



Proposed Condition Watershed Analysis Revised August 4, 2023

Type III 24-hr 10-yr Rainfall=5.19"

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Time span=0.00-40.00 hrs, dt=0.05 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: PR- 1/2 ROOF Runoff Area=1,391 sf 100.00% Impervious Runoff Depth=4.95"

Tc=6.0 min CN=98 Runoff=0.16 cfs 574 cf

Subcatchment 2S: PR-SWMA_R Runoff Area=11,800 sf 48.64% Impervious Runoff Depth=3.64"

Tc=6.0 min CN=86 Runoff=1.11 cfs 3,584 cf

Subcatchment 3S: Remaining Land Runoff Area=31,753 sf 0.00% Impervious Runoff Depth=2.18"

Flow Length=345' Tc=21.3 min CN=70 Runoff=1.20 cfs 5,764 cf

Subcatchment 4S: PR-YARD R Runoff Area=40,153 sf 0.00% Impervious Runoff Depth=2.43"

Flow Length=345' Slope=0.0350 '/' Tc=12.1 min CN=73 Runoff=2.12 cfs 8,132 cf

Pond 1P: Subsurface Drainage Structure Peak Elev=91.08' Storage=283 cf Inflow=0.16 cfs 574 cf

Outflow=0.01 cfs 574 cf

Pond 2P: SWMA Peak Elev=98.42' Storage=2,074 cf Inflow=1.11 cfs 3,584 cf

Discarded=0.04 cfs 3,584 cf Primary=0.00 cfs 0 cf Outflow=0.04 cfs 3,584 cf

Link 1L: Flow to the West Inflow=3.08 cfs 13,896 cf

Primary=3.08 cfs 13,896 cf

Total Runoff Area = 85,097 sf Runoff Volume = 18,054 cf Average Runoff Depth = 2.55" 91.62% Pervious = 77,967 sf 8.38% Impervious = 7,130 sf

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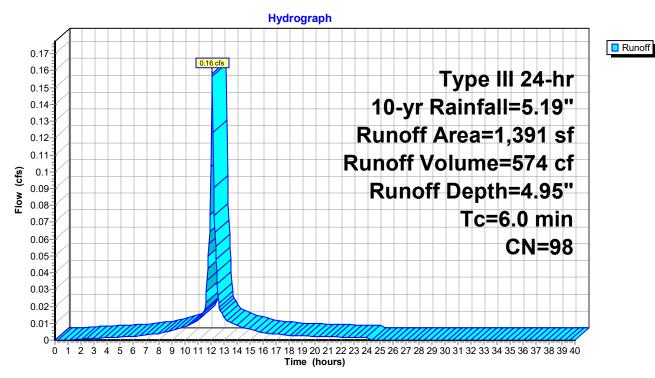
Summary for Subcatchment 1S: PR- 1/2 ROOF

Runoff = 0.16 cfs @ 12.09 hrs, Volume= 574 cf, Depth= 4.95" Routed to Pond 1P : Subsurface Drainage Structure

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Rainfall=5.19"

	Area (sf)	CN	Description		
	1,391	98	Roofs, HSG	G C	
	1,391		100.00% In	npervious A	Area
To	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0)				Direct Entry.

Subcatchment 1S: PR- 1/2 ROOF



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Summary for Subcatchment 2S: PR-SWMA_R

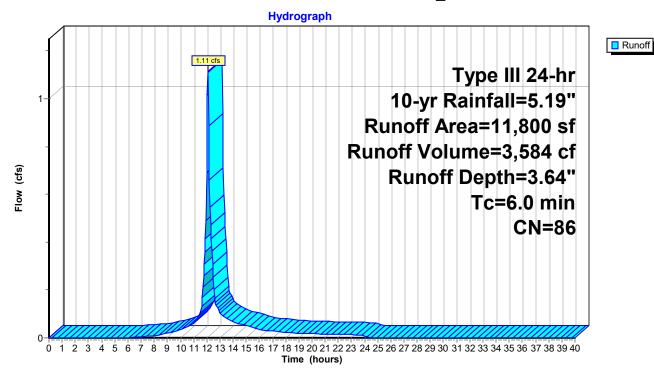
Runoff = 1.11 cfs @ 12.09 hrs, Volume= 3,584 cf, Depth= 3.64"

Routed to Pond 2P: SWMA

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Rainfall=5.19"

A	rea (sf)	CN	N Description				
	4,410	98	Paved park	ing, HSG C	C		
	6,061	74	>75% Gras	s cover, Go	lood, HSG C		
	1,329	98	Unconnecte	ed roofs, H	ISG C		
	11,800	86	Weighted A	verage			
	6,061		51.36% Per	vious Area	a		
	5,739		48.64% Imp	ervious Ar	rea		
	1,329		23.16% Und	connected			
_				_			
Tc	Length	Slope	•	Capacity	·		
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)			
6.0					Direct Entry,		

Subcatchment 2S: PR-SWMA_R



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Summary for Subcatchment 3S: Remaining Land

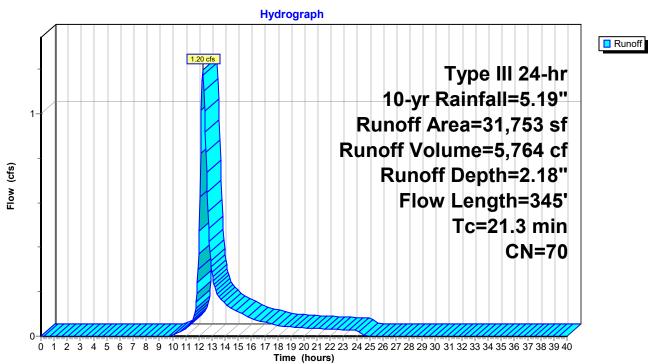
Runoff = 1.20 cfs @ 12.31 hrs, Volume= 5,764 cf, Depth= 2.18"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Rainfall=5.19"

_	Α	rea (sf)	CN E	Description		
		30,003	70 V	Voods, Go	od, HSG C	
_		1,750	74 >	75% Gras	s cover, Go	ood, HSG C
		31,753	70 V	Veighted A	verage	
		31,753	1	00.00% Pe	ervious Are	a
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	17.0	100	0.0350	0.10		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.28"
	4.3	245	0.0360	0.95		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	21.3	345	Total			

Subcatchment 3S: Remaining Land



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Summary for Subcatchment 4S: PR-YARD_R

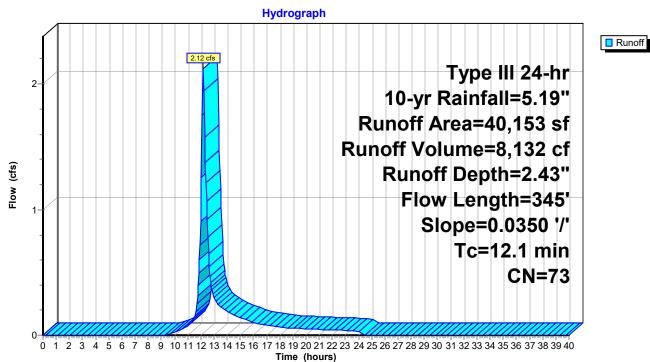
Runoff = 2.12 cfs @ 12.17 hrs, Volume= 8,132 cf, Depth= 2.43"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 10-yr Rainfall=5.19"

	Area (sf)	CN	Description			
	30,153	74	>75% Gras	s cover, Go	ood, HSG C	
	10,000	70	Woods, Go	od, HSG C		
	40,153	73	Weighted A	Average		
	40,153		100.00% P	ervious Are	a	
T	5		,	Capacity	Description	
(min	ı) (feet)	(ft/f	t) (ft/sec)	(cfs)		
7.	7 100	0.035	0 0.22		Sheet Flow,	
					Grass: Short n= 0.150 P2= 3.28"	
4.4	4 245	0.035	0 0.94		Shallow Concentrated Flow,	
					Woodland Kv= 5.0 fps	
12.	1 345	Total				

Subcatchment 4S: PR-YARD_R



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Type III 24-hr 10-yr Rainfall=5.19" Printed 8/14/2023

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Summary for Pond 1P: Subsurface Drainage Structure

Inflow Area = 1,391 sf,100.00% Impervious, Inflow Depth = 4.95" for 10-yr event

Inflow = 0.16 cfs @ 12.09 hrs, Volume= 574 cf

Outflow = 0.01 cfs @ 10.40 hrs, Volume= 574 cf, Atten= 96%, Lag= 0.0 min

Discarded = 0.01 cfs @ 10.40 hrs, Volume= 574 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Peak Elev= 91.08' @ 14.99 hrs Surf.Area= 274 sf Storage= 283 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 365.0 min (1,112.4 - 747.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	89.50'	253 cf	11.17'W x 24.50'L x 3.54'H Field A
			969 cf Overall - 335 cf Embedded = 634 cf x 40.0% Voids
#2A	90.00'	335 cf	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		590 of	Total Available Storage

589 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	89.50'	1.020 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.01 cfs @ 10.40 hrs HW=89.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.01 cfs)

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Pond 1P: Subsurface Drainage Structure - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

3 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 22.50' Row Length +12.0" End Stone x 2 = 24.50' Base Length

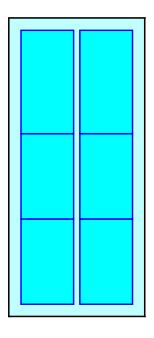
2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 335.3 cf Chamber Storage

968.9 cf Field - 335.3 cf Chambers = 633.6 cf Stone x 40.0% Voids = 253.5 cf Stone Storage

Chamber Storage + Stone Storage = 588.8 cf = 0.014 af Overall Storage Efficiency = 60.8% Overall System Size = 24.50' x 11.17' x 3.54'

6 Chambers 35.9 cy Field 23.5 cy Stone



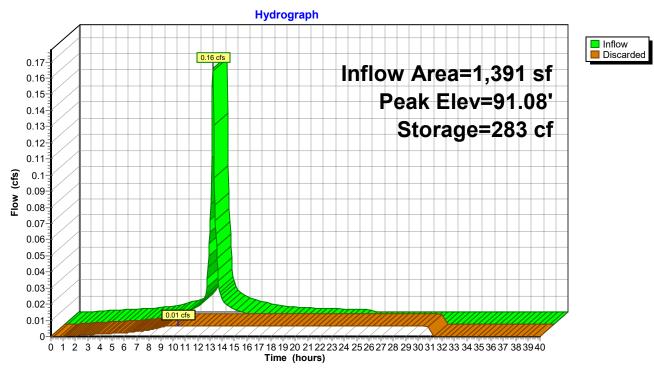


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Pond 1P: Subsurface Drainage Structure



Type III 24-hr 10-yr Rainfall=5.19" Printed 8/14/2023

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Summary for Pond 2P: SWMA

Inflow Area = 11,800 sf, 48.64% Impervious, Inflow Depth = 3.64" for 10-yr event Inflow = 1.11 cfs @ 12.09 hrs, Volume= 3,584 cf

Outflow = 0.04 cfs @ 15.55 hrs, Volume= 3,584 cf, Atten= 96%, Lag= 207.8 min Discarded = 0.04 cfs @ 15.55 hrs, Volume= 3,584 cf

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routed to Link 1L : Flow to the West

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Peak Elev= 98.42' @ 15.55 hrs Surf.Area= 1,782 sf Storage= 2,074 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 516.5 min (1,319.5 - 803.0)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	97.00'	6,99	00 cf Custom	n Stage Data (Pri	smatic) Listed below (Recalc)
Elevation (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
97.0	00	1,150	0	0	
98.0	00	1,580	1,365	1,365	
99.0	00	2,060	1,820	3,185	
100.0	00	2,600	2,330	5,515	
100.5	50	3,300	1,475	6,990	
Device	Routing	Invert	Outlet Device	es	
#1	Discarded	97.00'	1.020 in/hr E	xfiltration over S	Surface area
#2	Primary	99.25'	4.0" Round	Culvert	
			Inlet / Outlet		neadwall, Ke= 0.500 8.00' S= 0.0278 '/' Cc= 0.900

Discarded OutFlow Max=0.04 cfs @ 15.55 hrs HW=98.42' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=97.00' TW=0.00' (Dynamic Tailwater) 2=Culvert (Controls 0.00 cfs)

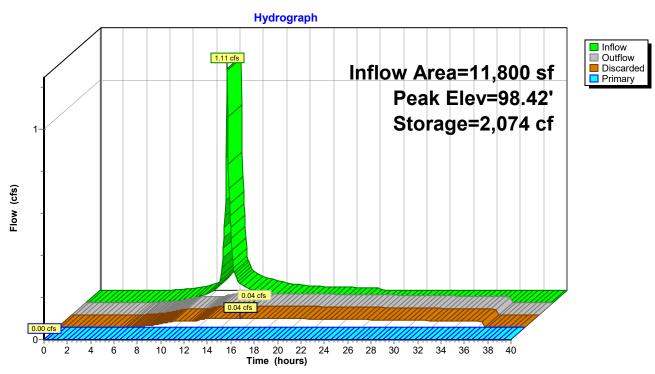
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Pond 2P: SWMA



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Summary for Link 1L: Flow to the West

Inflow Area = 83,706 sf, 6.86% Impervious, Inflow Depth = 1.99" for 10-yr event

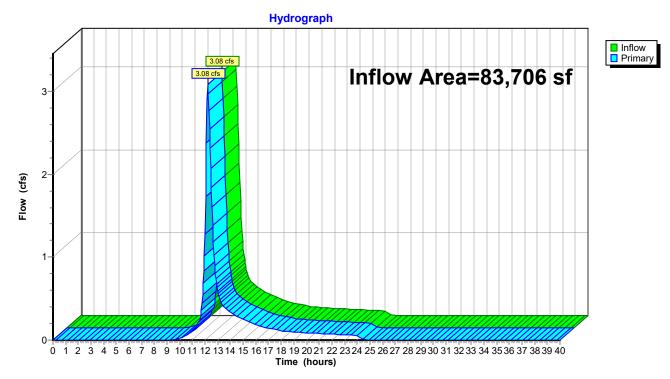
Inflow = 3.08 cfs @ 12.21 hrs, Volume= 13,896 cf

Primary = 3.08 cfs @ 12.21 hrs, Volume= 13,896 cf, Atten= 0%, Lag= 0.0 min

Routed to nonexistent node 3L

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs

Link 1L: Flow to the West



Proposed Condition Watershed Analysis Revised August 4, 2023

Type III 24-hr 100-yr Rainfall=8.21"

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Time span=0.00-40.00 hrs, dt=0.05 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: PR- 1/2 ROOF Runoff Area=1,391 sf 100.00% Impervious Runoff Depth=7.97"

Tc=6.0 min CN=98 Runoff=0.25 cfs 924 cf

Subcatchment 2S: PR-SWMA_R Runoff Area=11,800 sf 48.64% Impervious Runoff Depth=6.54"

Tc=6.0 min CN=86 Runoff=1.94 cfs 6,426 cf

Subcatchment 3S: Remaining Land Runoff Area=31,753 sf 0.00% Impervious Runoff Depth=4.65"

Flow Length=345' Tc=21.3 min CN=70 Runoff=2.60 cfs 12,292 cf

Subcatchment 4S: PR-YARD R Runoff Area=40,153 sf 0.00% Impervious Runoff Depth=5.00"

Flow Length=345' Slope=0.0350 '/' Tc=12.1 min CN=73 Runoff=4.39 cfs 16,719 cf

Pond 1P: Subsurface Drainage Structure Peak Elev=92.64' Storage=545 cf Inflow=0.25 cfs 924 cf

Outflow=0.01 cfs 827 cf

Peak Elev=99.37' Storage=3,985 cf Inflow=1.94 cfs 6,426 cf

Discarded=0.05 cfs 5,191 cf Primary=0.03 cfs 352 cf Outflow=0.09 cfs 5,543 cf

Link 1L: Flow to the West Inflow=6.52 cfs 29,363 cf

Primary=6.52 cfs 29,363 cf

Total Runoff Area = 85,097 sf Runoff Volume = 36,360 cf Average Runoff Depth = 5.13" 91.62% Pervious = 77,967 sf 8.38% Impervious = 7,130 sf HydroCAD® 10.20-2f s/n 06611 © 2022 HydroCAD Software Solutions LLC

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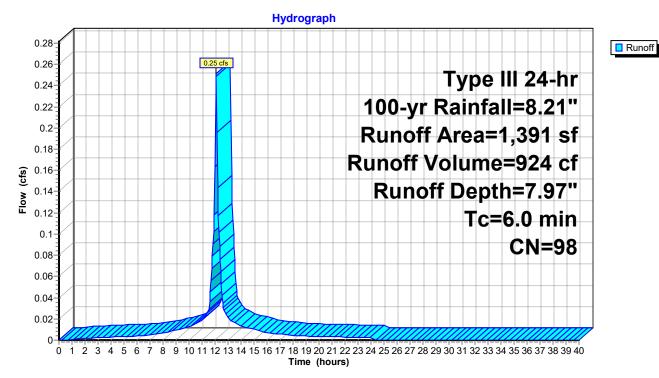
Summary for Subcatchment 1S: PR- 1/2 ROOF

Runoff = 0.25 cfs @ 12.09 hrs, Volume= 924 cf, Depth= 7.97" Routed to Pond 1P : Subsurface Drainage Structure

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 100-yr Rainfall=8.21"

	Area (sf)	CN	Description		
	1,391	98	Roofs, HSC	G C	
•	1,391		100.00% In	npervious A	Area
Tc	Length	Slope	· Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	•	(cfs)	
6.0					Direct Entry.

Subcatchment 1S: PR- 1/2 ROOF



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Summary for Subcatchment 2S: PR-SWMA_R

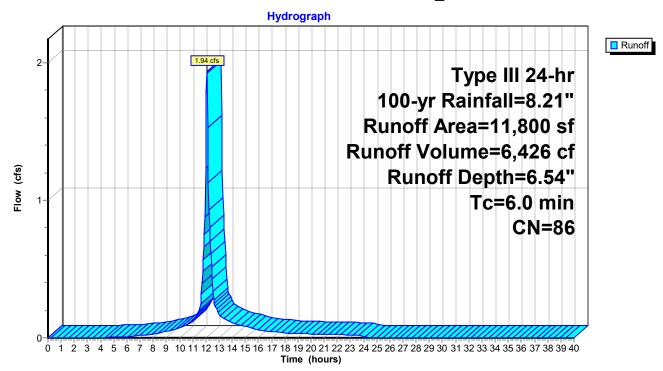
Runoff = 1.94 cfs @ 12.09 hrs, Volume= 6,426 cf, Depth= 6.54"

Routed to Pond 2P: SWMA

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 100-yr Rainfall=8.21"

A	rea (sf)	CN	N Description				
	4,410	98	Paved park	ing, HSG C	C		
	6,061	74	>75% Gras	s cover, Go	lood, HSG C		
	1,329	98	Unconnecte	ed roofs, H	ISG C		
	11,800	86	Weighted A	verage			
	6,061		51.36% Per	vious Area	a		
	5,739		48.64% Imp	ervious Ar	rea		
	1,329		23.16% Und	connected			
_				_			
Tc	Length	Slope	•	Capacity	·		
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)			
6.0					Direct Entry,		

Subcatchment 2S: PR-SWMA_R



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Runoff

Summary for Subcatchment 3S: Remaining Land

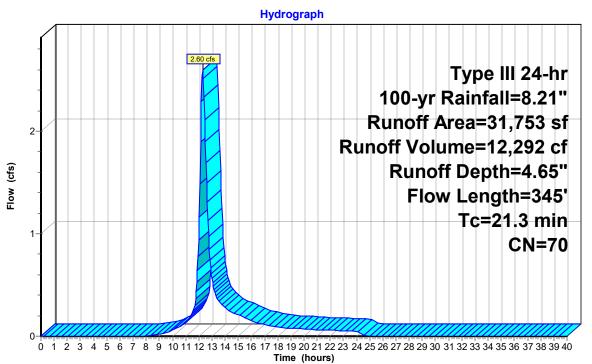
Runoff = 2.60 cfs @ 12.30 hrs, Volume= 12,292 cf, Depth= 4.65"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 100-yr Rainfall=8.21"

	rea (sf)	CN [Description		
	30,003	70 \	Noods, Go	od, HSG C	
	1,750	74 >	>75% Gras	s cover, Go	ood, HSG C
	31,753	70 \	Neighted A	verage	
	31,753	•	100.00% Pe	ervious Are	a
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
17.0	100	0.0350	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.28"
4.3	245	0.0360	0.95		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
21.3	345	Total			

Subcatchment 3S: Remaining Land



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Summary for Subcatchment 4S: PR-YARD_R

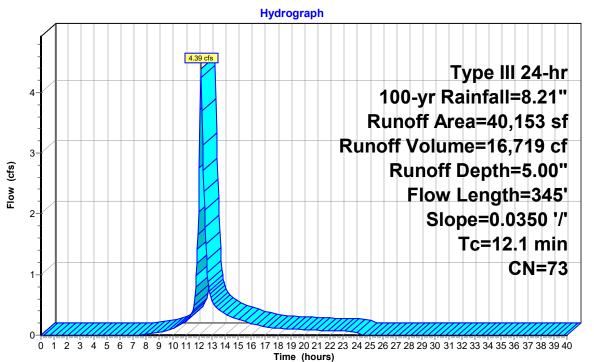
Runoff = 4.39 cfs @ 12.17 hrs, Volume= 16,719 cf, Depth= 5.00"

Routed to Link 1L: Flow to the West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Type III 24-hr 100-yr Rainfall=8.21"

	\rea (sf)	CN I	Description					
	30,153	74	>75% Gras	s cover, Go	ood, HSG C			
	10,000	70	Woods, Go	od, HSG C				
	40,153	73	Weighted A	verage				
	40,153		100.00% Pe	ervious Are	a			
Tc	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
7.7	100	0.0350	0.22		Sheet Flow,			
					Grass: Short n= 0.150 P2= 3.28"			
4.4	245	0.0350	0.94		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
12.1	345	Total						

Subcatchment 4S: PR-YARD_R





PROPOSED_R

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Summary for Pond 1P: Subsurface Drainage Structure

Inflow Area = 1,391 sf,100.00% Impervious, Inflow Depth = 7.97" for 100-yr event

Inflow = 0.25 cfs @ 12.09 hrs, Volume= 924 cf

Outflow = 0.01 cfs @ 8.90 hrs, Volume= 827 cf, Atten= 97%, Lag= 0.0 min

Discarded = 0.01 cfs @ 8.90 hrs, Volume= 827 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Peak Elev= 92.64' @ 16.40 hrs Surf.Area= 274 sf Storage= 545 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 588.6 min (1,329.5 - 740.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	89.50'	253 cf	11.17'W x 24.50'L x 3.54'H Field A
			969 cf Overall - 335 cf Embedded = 634 cf x 40.0% Voids
#2A	90.00'	335 cf	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		589 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	89.50'	1.020 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.01 cfs @ 8.90 hrs HW=89.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.01 cfs)

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Pond 1P: Subsurface Drainage Structure - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

3 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 22.50' Row Length +12.0" End Stone x 2 = 24.50' Base Length

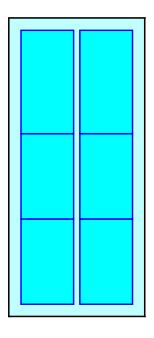
2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

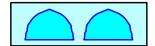
6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 335.3 cf Chamber Storage

968.9 cf Field - 335.3 cf Chambers = 633.6 cf Stone x 40.0% Voids = 253.5 cf Stone Storage

Chamber Storage + Stone Storage = 588.8 cf = 0.014 af Overall Storage Efficiency = 60.8% Overall System Size = 24.50' x 11.17' x 3.54'

6 Chambers 35.9 cy Field 23.5 cy Stone



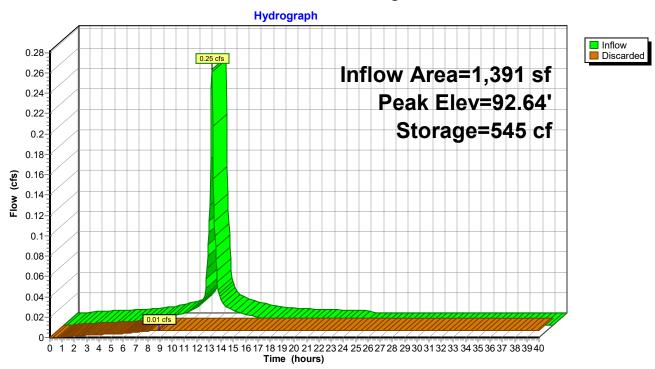


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Pond 1P: Subsurface Drainage Structure



Volume

Type III 24-hr 100-yr Rainfall=8.21"

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Invert

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Summary for Pond 2P: SWMA

Inflow Area = 11,800 sf, 48.64% Impervious, Inflow Depth = 6.54" for 100-yr event Inflow = 1.94 cfs @ 12.09 hrs, Volume= 6,426 cf

Outflow = 0.09 cfs @ 14.85 hrs, Volume= 5,543 cf, Atten= 96%, Lag= 165.6 min Discarded = 0.05 cfs @ 14.85 hrs, Volume= 5,191 cf

Primary = 0.03 cfs @ 14.85 hrs, Volume= 352 cf

Routed to Link 1L : Flow to the West

Routing by Dyn-Stor-Ind method, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs Peak Elev= 99.37' @ 14.85 hrs Surf.Area= 2,260 sf Storage= 3,985 cf

Plug-Flow detention time= 637.8 min calculated for 5,543 cf (86% of inflow) Center-of-Mass det. time= 577.5 min (1,364.4 - 786.9)

Avail Storage Storage Description

Volume	IIIVEIL	Avaii.0t0i	age Storage	Description			
#1	97.00'	6,99	00 cf Custom	Stage Data (Pris	matic) Listed below (Recalc)		
Elevation	on Su	ırf.Area	Inc.Store	Cum.Store			
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
97.0	00	1,150	0	0			
98.0	00	1,580	1,365	1,365			
99.0	00	2,060	1,820	3,185			
100.0	00	2,600	2,330	5,515			
100.5	50	3,300	1,475	6,990			
Device	Routing	Invert	Outlet Device	es			
#1	Discarded	97.00'	1.020 in/hr Exfiltration over Surface area				
#2	Primary	ary 99.25' 4.0" Round Culvert					
	L= 45.0' CPP, square edge headwall, Ke= 0.500						
			Inlet / Outlet Invert= 99.25' / 98.00' S= 0.0278 '/' Cc= 0.900				
			n= 0.010, Flo	ow Area= 0.09 sf			

Discarded OutFlow Max=0.05 cfs @ 14.85 hrs HW=99.37' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=0.03 cfs @ 14.85 hrs HW=99.37' TW=0.00' (Dynamic Tailwater) 2=Culvert (Inlet Controls 0.03 cfs @ 1.18 fps)

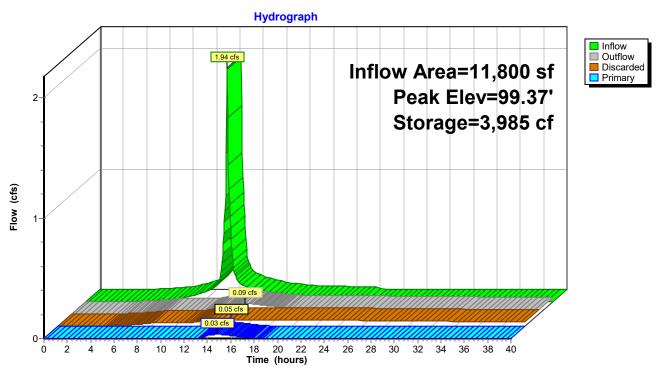
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Pond 2P: SWMA



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Summary for Link 1L: Flow to the West

Inflow Area = 83,706 sf, 6.86% Impervious, Inflow Depth = 4.21" for 100-yr event

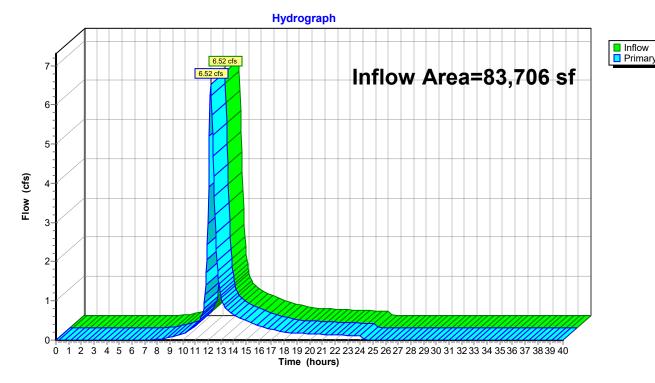
Inflow = 6.52 cfs @ 12.20 hrs, Volume= 29,363 cf

Primary = 6.52 cfs @ 12.20 hrs, Volume= 29,363 cf, Atten= 0%, Lag= 0.0 min

Routed to nonexistent node 3L

Primary outflow = Inflow, Time Span= 0.00-40.00 hrs, dt= 0.05 hrs

Link 1L: Flow to the West



| Long Term Operation & Maintenance Plan - No Change

This Operation & Maintenance Plan is prepared to comply with provisions set forth in the Massachusetts Department of Environmental Protection (MassDEP) Stormwater Management Standards.

Structural Best Management Practices (BMPs) require periodic maintenance to ensure proper function and efficiency in pollutant removal from stormwater discharges that would otherwise reach wetland resource areas untreated. Maintenance schedules found below are as recommended in MassDEP's Massachusetts Stormwater Handbook and/or as recommended in the manufacturer's specifications.

The following BMP provides groundwater recharge

Subsurface Infiltration Chambers - Pond 1P

Chamber maintenance is not generally required. However, recharge systems are prone to failure due to clogging. Regulating the sediment and petroleum product input into the proposed recharge system is the priority maintenance activity. Sediments and any oil spillage should be trapped and removed before they reach the chambers. Any upstream devices connected to the infiltration system (catch basins, deep sump manholes, proprietary devices) shall be inspected and cleaned at least twice per year to prevent sediments and debris from entering and clogging the recharge system.

Sediments must also be removed whenever the depth of deposits is greater than or equal to 3".

The contractor shall verify that the required washed crushed stone and geotechnical fabric materials are clean and free of sediments and petroleum residue prior to, during and after chamber system installation. Inspections of the chamber system shall be made by after every major storm for the first few months after construction to verify that proper functioning has been achieved. During the initial inspection the water level should be measured and recorded in a permanent log over several days to check the drainage duration and verify that sediments are not accumulating. If ponded water is present after 24 hours or an accumulation of sediment or debris is noted within the chambers the owner or designated property manager and engineer shall determine the cause for this condition and devise an action plan to improve system functionality.

Once the chamber system has been verified to perform as designed, interior chamber conditions shall be inspected at least twice per year. Post construction inspections (to be conducted through inspection ports) shall consist of documenting interior and stone bed conditions, measured water depth and presence of sediment. Should inspection indicate that the system is clogged (ponding water present after 24 hours and/or sediment accumulations) replacement or major repair actions may be required. Should the system require replacement or major repair actions the owner or designated property manager and engineer shall determine the cause for this condition and devise an action plan

The inspection and maintenance of the subsurface infiltration system shall belong to the owner or designated property manager.

Stormwater Management Area-Pond 2P

Basins are prone to clogging and failure so it is imperative to develop and implement aggressive maintenance plans and schedules. If required, installing the required pretreatment BMPs, e.g. deep-sump catch basins and sediment forebays, will significantly reduce the maintenance requirements for the basin.

Inspections and preventative maintenance shall be performed at least twice a year, and after every time drainage discharges through the high outlet orifice or a major storm event which is defined as a storm that is equal to or greater than the 2-year, 24-hour storm (3.1 inches in a 24-hour storm).

After the basin is on line, inspect it after every major storm for the first few months to ensure that it is stabilized and functioning properly. Take corrective action if necessary.

Note the time that water remains standing in the basin after a storm event. Standing water within the basin 48 to 72 hours after a storm indicates that the infiltration capacity of the basin may have been overestimated or the bottom has been clogged.

If the reason is clogging, determine the cause, e.g. erosion, excessive compaction, or low spots and take the necessary corrective action. Thereafter, inspect the infiltration basin at least twice per year.

Important items to check during the inspections include:

- 1. Signs of differential settlement,
- 2. Cracking,
- 3. Erosion,
- 4. Leakage in the embankments,
- 5. Tree growth on the embankments,
- 6. Condition of riprap,
- 7. Sediment accumulation and,
- 8. Health of the turf.

At least twice a year the buffer area, side slopes, and basin bottom shall be mowed. Remove the grass clippings and accumulated organic matter to prevent an impervious organic mat from forming. Remove trash and debris at this time as well as using deep tilling to break up any clogged surfaces, revegetate immediately.

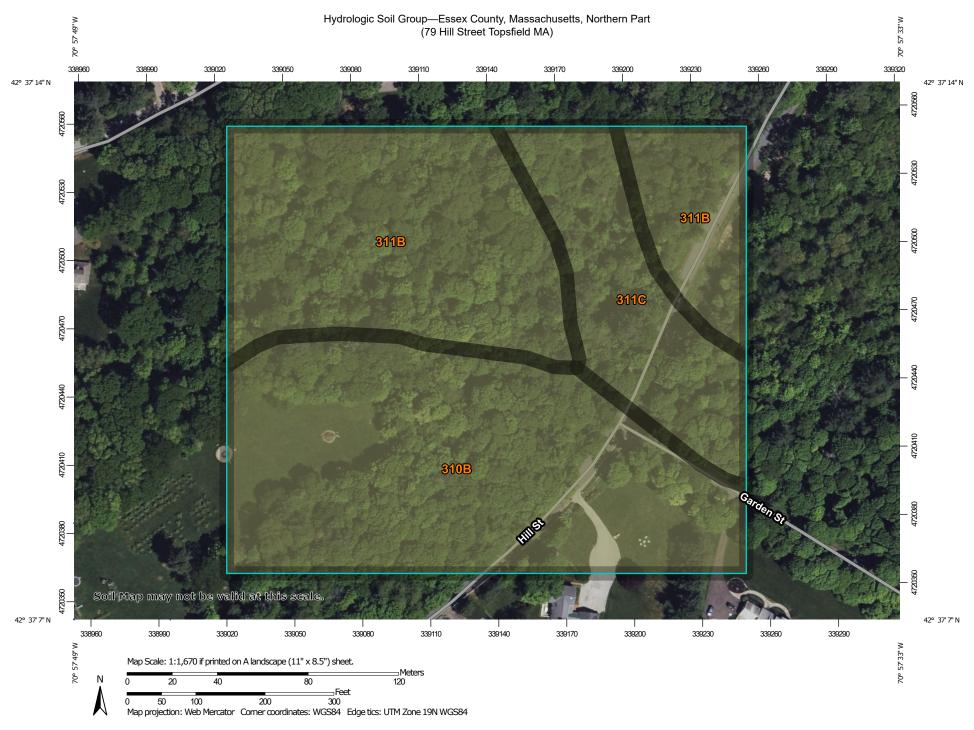
Remove sediment from the basin as necessary only when the floor of the basin is completely dry. Use light equipment to remove the top layer to prevent compacting the underlying soil. Deep till the remaining soil and revegetate as soon as possible.

	l Maintenance l							
Refer to Sections	s above for frequer	ncy of inspection						
Inspector:			Date:					
Inspector Title:								
Days since last r	rainfall:		Amount of last rainfall:					
Structural Controls: Subsurface Drainage Structure								
Structure Identification	Location	Condition Stone Bed	Settlement over system	Sediment Buildup in Basin				
Pond 1P	Rear of house	Poor Fair Good	Yes No	Minor□ Moderate□ Major□				
				Minor□ Moderate□ Major□				
				Minor□ Moderate□ Major□				
				Minor□ Moderate□ Major□				
				Minor□ Moderate□ Major□				
				Minor□ Moderate□ Major□				
Maintenance rec	quired							
To be performed	l by:		On or be	efore:				



Inspection and Maint Refer to Sections above for		ection		
Inspector:			Date:	
Inspector Title:				
Days since last rainfall:			Amount of last rainfall:	
Structural Controls:	Stormwater Man	agement Area		
Structure Identification	Location	Condition of side slope % vegetated	Sediment buildup in basin % accumulation	Rilling or gullying
Pond 2P	Front of house			Minor□ Moderate□ Major□
				Minor□ Moderate□ Major□
				Minor□ Moderate□ Major□
				Minor□ Moderate□ Major□
Maintenance required				,
To be performed by:			On or before	e:





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:15.800. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Essex County, Massachusetts, Northern Part Survey Area Data: Version 18, Sep 9, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: May 22, 2022—Jun 5. 2022 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
310B	Woodbridge fine sandy loam, 3 to 8 percent slopes	C/D	5.0	44.4%
311B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	C/D	4.4	39.2%
311C	Woodbridge fine sandy loam, 8 to 15 percent slopes, very stony	C/D	1.8	16.4%
Totals for Area of Inter	rest	11.2	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



NOAA Atlas 14, Volume 10, Version 3 Location name: Topsfield, Massachusetts, USA* Latitude: 42.6184°, Longitude: -70.9633° Elevation: 135.81 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

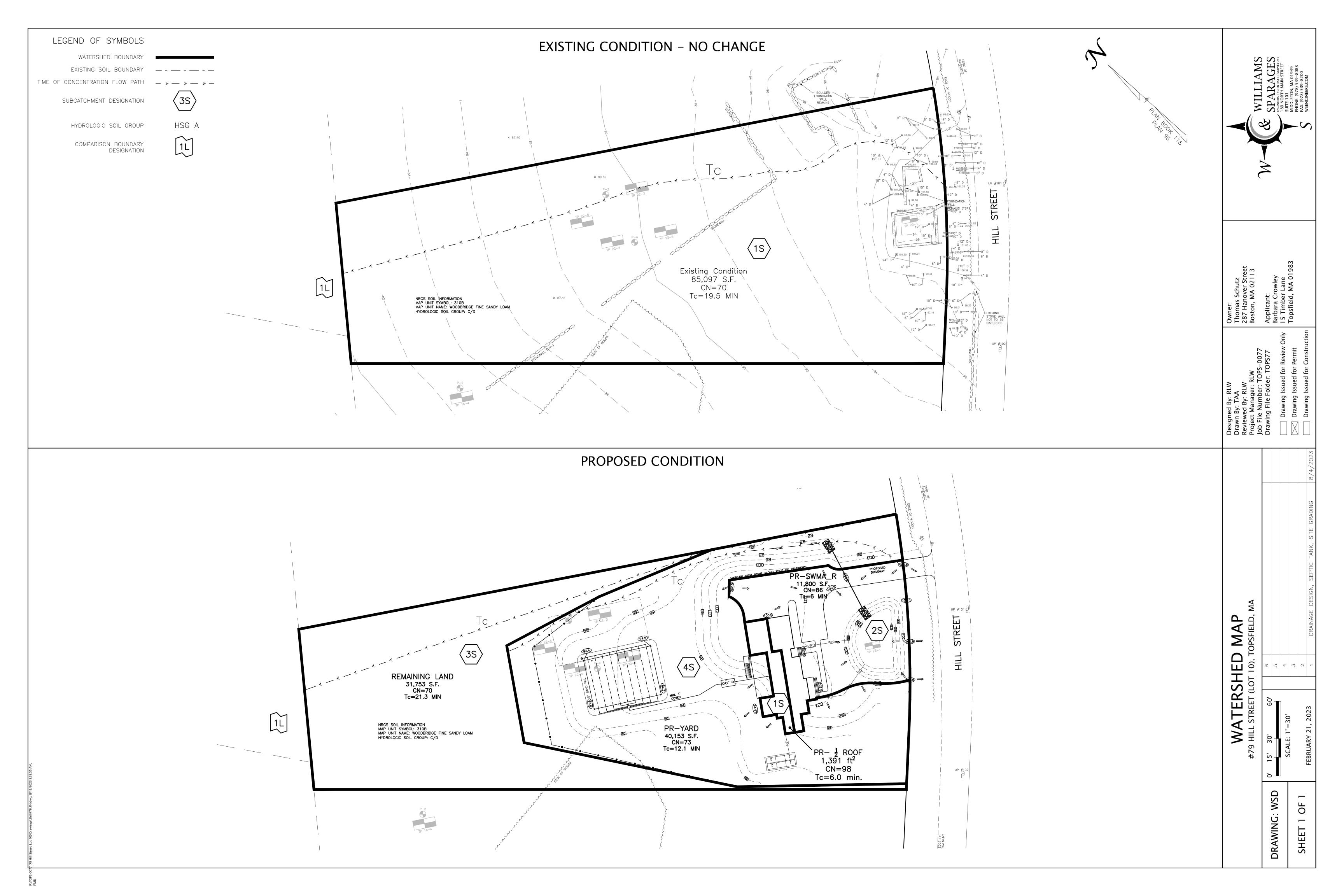
PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹ Average recurrence interval (years)										
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.311 (0.241-0.390)	0.374 (0.289-0.469)	0.476 (0.367-0.599)	0.561 (0.430-0.710)	0.677 (0.504-0.895)	0.765 (0.557-1.03)	0.857 (0.608-1.20)	0.961 (0.647-1.38)	1.11 (0.720-1.64)	1.23 (0.781-1.86)
10-min	0.441 (0.342-0.553)	0.530 (0.410-0.665)	0.675 (0.521-0.850)	0.795 (0.610-1.01)	0.960 (0.714-1.27)	1.08 (0.791-1.46)	1.21 (0.861-1.70)	1.36 (0.915-1.95)	1.57 (1.02-2.33)	1.75 (1.11-2.64)
15-min	0.519 (0.402-0.650)	0.623 (0.482-0.782)	0.793 (0.612-0.999)	0.934 (0.717-1.18)	1.13 (0.840-1.49)	1.27 (0.929-1.72)	1.43 (1.01-2.00)	1.60 (1.08-2.29)	1.85 (1.20-2.74)	2.06 (1.30-3.10)
30-min	0.716 (0.554-0.897)	0.858 (0.664-1.08)	1.09 (0.840-1.37)	1.28 (0.983-1.62)	1.55 (1.15-2.05)	1.75 (1.27-2.36)	1.96 (1.39-2.74)	2.19 (1.48-3.14)	2.54 (1.64-3.75)	2.82 (1.78-4.25)
60-min	0.913 (0.707-1.14)	1.09 (0.845-1.37)	1.39 (1.07-1.74)	1.63 (1.25-2.06)	1.97 (1.46-2.60)	2.22 (1.62-3.00)	2.48 (1.76-3.48)	2.79 (1.87-3.98)	3.22 (2.09-4.77)	3.58 (2.27-5.41)
2-hr	1.18 (0.919-1.47)	1.43 (1.11-1.78)	1.84 (1.43-2.30)	2.17 (1.68-2.74)	2.64 (1.99-3.49)	2.99 (2.20-4.03)	3.36 (2.42-4.73)	3.82 (2.57-5.43)	4.50 (2.93-6.62)	5.09 (3.23-7.63)
3-hr	1.36 (1.07-1.69)	1.66 (1.30-2.06)	2.15 (1.68-2.68)	2.56 (1.99-3.20)	3.11 (2.35-4.10)	3.53 (2.61-4.75)	3.98 (2.88-5.59)	4.53 (3.06-6.42)	5.38 (3.50-7.89)	6.12 (3.90-9.15)
6-hr	1.75 (1.39-2.16)	2.14 (1.69-2.64)	2.78 (2.19-3.44)	3.31 (2.60-4.13)	4.05 (3.08-5.30)	4.58 (3.42-6.15)	5.17 (3.77-7.24)	5.91 (4.01-8.32)	7.05 (4.60-10.3)	8.04 (5.13-11.9)
12-hr	2.21 (1.77-2.71)	2.71 (2.16-3.33)	3.53 (2.80-4.34)	4.20 (3.32-5.20)	5.13 (3.93-6.67)	5.82 (4.37-7.74)	6.57 (4.81-9.11)	7.49 (5.11-10.5)	8.91 (5.84-12.9)	10.1 (6.49-14.9)
24-hr	2.65 (2.14-3.23)	3.29 (2.65-4.00)	4.33 (3.47-5.29)	5.19 (4.13-6.37)	6.38 (4.92-8.24)	7.25 (5.49-9.60)	8.21 (6.06-11.4)	9.40 (6.44-13.1)	11.3 (7.42-16.2)	12.9 (8.29-18.9)
2-day	3.02 (2.45-3.65)	3.82 (3.10-4.62)	5.12 (4.14-6.21)	6.20 (4.98-7.57)	7.69 (6.00-9.91)	8.77 (6.71-11.6)	9.98 (7.46-13.8)	11.6 (7.95-16.0)	14.1 (9.29-20.1)	16.3 (10.5-23.7)
3-day	3.32 (2.71-3.99)	4.18 (3.41-5.03)	5.58 (4.53-6.75)	6.74 (5.45-8.20)	8.35 (6.54-10.7)	9.51 (7.31-12.5)	10.8 (8.12-14.9)	12.5 (8.63-17.2)	15.3 (10.1-21.7)	17.7 (11.4-25.7)
4-day	3.60 (2.95-4.32)	4.49 (3.67-5.39)	5.93 (4.84-7.15)	7.13 (5.78-8.64)	8.78 (6.90-11.2)	9.98 (7.70-13.1)	11.3 (8.53-15.6)	13.1 (9.04-18.0)	15.9 (10.6-22.6)	18.5 (11.9-26.7)
7-day	4.38 (3.61-5.22)	5.29 (4.36-6.32)	6.79 (5.57-8.14)	8.03 (6.55-9.68)	9.73 (7.69-12.4)	11.0 (8.50-14.3)	12.4 (9.33-16.9)	14.2 (9.84-19.3)	17.1 (11.4-24.1)	19.7 (12.7-28.3)
10-day	5.07 (4.21-6.03)	6.01 (4.98-7.16)	7.54 (6.22-9.01)	8.81 (7.22-10.6)	10.6 (8.37-13.3)	11.8 (9.19-15.3)	13.3 (10.0-17.9)	15.1 (10.5-20.5)	17.9 (11.9-25.2)	20.5 (13.3-29.3)
20-day	7.03 (5.88-8.30)	8.05 (6.73-9.53)	9.73 (8.10-11.5)	11.1 (9.20-13.3)	13.0 (10.4-16.2)	14.5 (11.2-18.4)	16.0 (12.0-21.1)	17.8 (12.5-23.9)	20.3 (13.6-28.3)	22.5 (14.6-32.0)
30-day	8.64 (7.27-10.2)	9.74 (8.19-11.5)	11.5 (9.66-13.6)	13.0 (10.8-15.5)	15.1 (12.0-18.6)	16.7 (12.9-21.0)	18.3 (13.6-23.7)	20.0 (14.1-26.7)	22.3 (15.0-31.0)	24.2 (15.8-34.3)
45-day	10.7 (9.04-12.5)	11.9 (10.0-13.9)	13.8 (11.6-16.2)	15.4 (12.9-18.2)	17.6 (14.1-21.6)	19.3 (15.0-24.1)	21.0 (15.6-27.0)	22.7 (16.1-30.2)	24.9 (16.8-34.3)	26.5 (17.3-37.3)
60-day	12.4 (10.6-14.5)	13.7 (11.6-16.0)	15.7 (13.3-18.4)	17.4 (14.6-20.5)	19.7 (15.8-24.0)	21.5 (16.8-26.7)	23.3 (17.3-29.7)	24.9 (17.7-33.1)	27.0 (18.3-37.1)	28.5 (18.6-40.0)

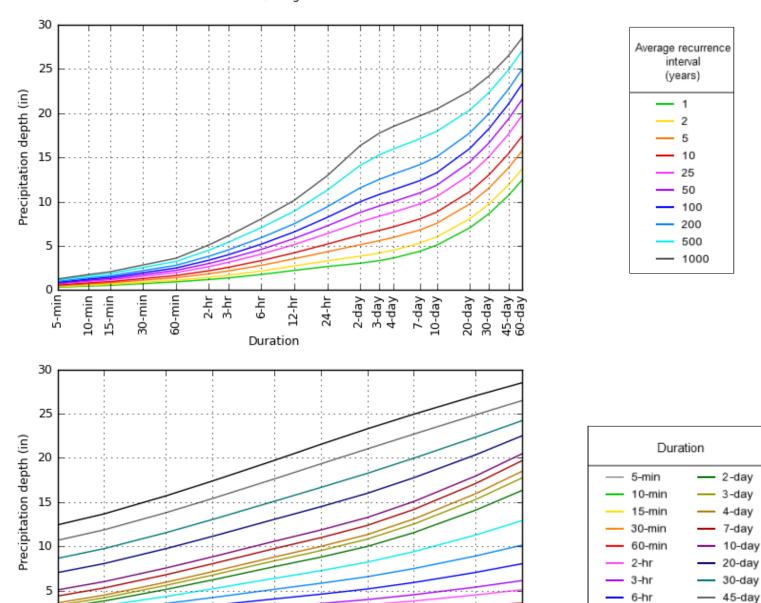
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PDS-based depth-duration-frequency (DDF) curves Latitude: 42.6184°, Longitude: -70.9633°



NOAA Atlas 14, Volume 10, Version 3

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Average recurrence interval (years)

01

Created (GMT): Thu Feb 16 15:10:42 2023

500

1000

12-hr

24-hr

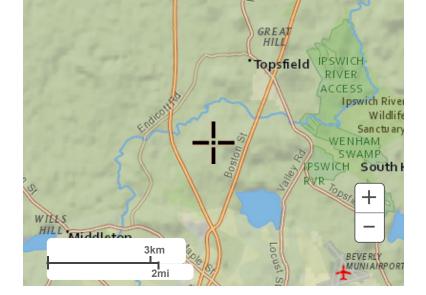
- 60-day

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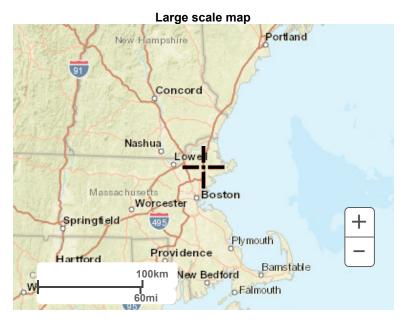
200

Maps & aerials

Small scale terrain



Large scale terrain Portland Concord G uM NEW HAMPSHIRE Nashua Worcester Boston SSACHUSETTS ringfield Plymouth Cape Cod Bay Barnstable Providence ew Bedford 100km 60mi Falmouth



Large scale aerial



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